

A Reciprocity Theorem for the Interaction of Electromagnetic Plane Waves with a One-Dimensional Inhomogeneous Slab*

The geometry of the problem is shown in Fig. 1. A plane wave, varying in time as $e^{-i\omega t}$, with components E_{\parallel} and $E_{\perp} = E_{\perp}$ is incident at an angle θ upon an inhomogeneous slab at the boundary $z=0$. The complex index of refraction of the medium, $n(z)$ and its derivative varies continuously in a direction normal to the boundaries. E_{\parallel} and E_{\perp} are reflected components, and E_{\parallel} and E_{\perp} are transmitted components of the electric vector. Comparison of these solutions with those generated by inverting the slab will establish a reciprocity criteria. This inversion procedure is equivalent to analyzing two-way transmission through a given inhomogeneous slab.

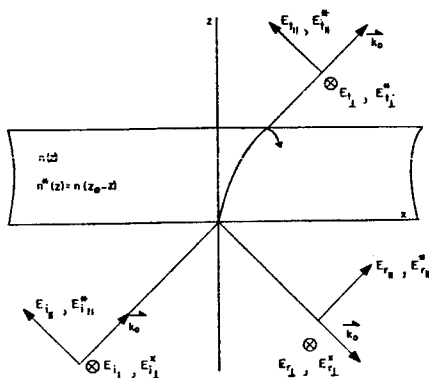


Fig. 1.

Stratton¹ has shown that the solutions to the wave equation are uniquely described by those components of the electric vector which are perpendicular to and parallel to the plane of incidence, which is that plane containing the propagation vector, k_0 and the vector normal to the boundaries of the slab. Since the parallel component of the electric vector is related to the y component of the magnetic vector, H_y , the properties are completely defined by the wave equations for E_y and H_y . These equations for a medium which is inhomogeneous along z are

$$\frac{d^2 E_y(z)}{dz^2} + k_0^2 [n^2(z) - \sin^2 \theta] E_y(z) = 0 \quad (1)$$

$$\frac{d^2 H_y(z)}{dz^2} - \frac{1}{n^2(z)} \frac{dn^2(z)}{dz} \frac{dH_y(z)}{dz} + k_0^2 [n^2(z) - \sin^2 \theta] H_y(z) = 0. \quad (2)$$

The solutions to these equations are of the form

* Received April 19, 1963. After this derivation was completed, it was discovered that a reciprocity relationship was stated for a plane wave normally incident upon an N-layer dielectric (R. Hollis, "Reciprocal relationships in an n-slab dielectric," *Proc. IRE (Correspondence)*, vol. 49, p. 1579; October, 1961). This paper presents a more general picture by considering continuous variation of the material properties and angle of incidence.
1. J. A. Stratton, "Electromagnetic Theory," McGraw-Hill Book Company, Inc., New York, N. Y. p. 492; 1941.

$$\begin{aligned} \frac{E_y}{E_{0y}} &= C_1 u_1(z) + C_2 u_2(z); \\ \frac{H_y}{H_{0y}} &= C_3 v_1(z) + C_4 v_2(z), \end{aligned} \quad (3)$$

where E_{0y} and H_{0y} are the amplitudes of the incident E and H vectors and the C 's are constants. Continuity of the tangential components of E and H at $z=0$ and $z=z_0$, lead to the following boundary conditions for (1) and (2):

$$\begin{bmatrix} u_1(0) & u_2(0) & -1 & 0 \\ u_1'(0) & u_2'(0) & jk_0 \cos \theta & 0 \\ u_1(z_0) & u_2(z_0) & 0 & -e^{jk_0 z_0} \cos \theta \\ u_1'(z_0) & u_2'(z_0) & 0 & -jk_0 \cos \theta e^{jk_0 z_0} \cos \theta \end{bmatrix} \begin{bmatrix} C_1 \\ C_2 \\ R_{\perp} \\ T_{\perp} \end{bmatrix} = \begin{bmatrix} 1 \\ jk_0 \cos \theta \\ 0 \\ 0 \end{bmatrix} \quad (4)$$

$$\begin{bmatrix} v_1(0) & v_2(0) & -1 & 0 \\ v_1'(0) & v_2'(0) & jk_0 n^2(0) \cos \theta & 0 \\ v_1(z_0) & v_2(z_0) & 0 & -e^{jk_0 z_0} \cos \theta \\ v_1'(z_0) & v_2'(z_0) & 0 & -jk_0 n^2(z_0) \cos \theta e^{jk_0 z_0} \cos \theta \end{bmatrix} \begin{bmatrix} C_3 \\ C_4 \\ R_{\parallel} \\ T_{\parallel} \end{bmatrix} = \begin{bmatrix} 1 \\ jk_0 n^2(0) \cos \theta \\ 0 \\ 0 \end{bmatrix} \quad (5)$$

The R 's and T 's are the complex reflection and transmission coefficients, respectively; and k_0 is the wave number of the incident wave. A medium whose index of refraction is $n^*(z)$ results in identical boundary conditions except the R 's, T 's, C 's, u 's, v 's, and n 's are superscripted by a star (*). The index of refraction, $n^*(z)$ of a slab which is inverted may be defined in terms of the given value of $n(z)$ such that $n^*(z) = n(z_0 - z)$. Consequently, the solutions of the inverted slab become

$$\begin{aligned} u_1^*(z) &= u_1(z_0 - z); & u_2^*(z) &= u_2(z_0 - z) \\ v_1^*(z) &= v_1(z_0 - z); & v_2^*(z) &= v_2(z_0 - z), \end{aligned} \quad (6)$$

and the boundary conditions for the starred solutions become

$$\begin{bmatrix} u_1(0) & u_2(0) & 0 & -e^{jk_0 z_0} \cos \theta \\ u_1'(0) & u_2'(0) & 0 & jk_0 \cos \theta e^{jk_0 z_0} \cos \theta \\ u_1(z_0) & u_2(z_0) & -1 & 0 \\ u_1'(z_0) & u_2'(z_0) & -jk_0 \cos \theta & 0 \end{bmatrix} \begin{bmatrix} C_1^* \\ C_2^* \\ R_{\perp}^* \\ T_{\perp}^* \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ -jk_0 \cos \theta \end{bmatrix} \quad (7)$$

$$\begin{bmatrix} v_1(0) & v_2(0) & 0 & -e^{jk_0 z_0} \cos \theta \\ v_1'(0) & v_2'(0) & 0 & jk_0 n^2(0) \cos \theta e^{jk_0 z_0} \cos \theta \\ v_1(z_0) & v_2(z_0) & -1 & 0 \\ v_1'(z_0) & v_2'(z_0) & -jk_0 n^2(z_0) \cos \theta & 0 \end{bmatrix} \begin{bmatrix} C_3^* \\ C_4^* \\ R_{\parallel}^* \\ T_{\parallel}^* \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ -jk_0 n^2(z_0) \cos \theta \end{bmatrix} \quad (8)$$

Let the determinants of the matrix equations (4), (5), (7), and (8) be Δ_1 , Δ_2 , Δ_1^* , and Δ_2^* , respectively. Expansion of the determinants shows that $\Delta_1 = -\Delta_1^*$ and $\Delta_2 = -\Delta_2^*$. The reflection and transmission coefficients can be solved in terms of Δ_1 and Δ_2 ; however, the following difference relationships are the quantities of interest:

$$\Delta_1(T_{\perp} - T_{\perp}^*) = -2jk_0 \cos \theta \left\{ \begin{vmatrix} u_1(z_0) & u_2(z_0) \\ u_1'(z_0) & u_2'(z_0) \end{vmatrix} - \begin{vmatrix} u_1(0) & u_2(0) \\ u_1'(0) & u_2'(0) \end{vmatrix} \right\} \quad (9)$$

$$\Delta_2(T_{\parallel} - T_{\parallel}^*) = -2jk_0 \cos \theta \left\{ n^2(0) \begin{vmatrix} v_1(z_0) & v_2(z_0) \\ v_1'(z_0) & v_2'(z_0) \end{vmatrix} - n^2(z_0) \begin{vmatrix} v_1(0) & v_2(0) \\ v_1'(0) & v_2'(0) \end{vmatrix} \right\} \quad (10)$$

$$\Delta_1(R_{\perp} - R_{\perp}^*) = -2jk_0 \cos \theta e^{jk_0 z_0} \cos \theta \left\{ \begin{vmatrix} u_1(0) & u_2(0) \\ u_1'(0) & u_2'(0) \end{vmatrix} - \begin{vmatrix} u_1(z_0) & u_2(z_0) \\ u_1'(z_0) & u_2'(z_0) \end{vmatrix} \right\} \quad (11)$$

$$\Delta_2(R_{\parallel} - R_{\parallel}^*) = -2jk_0 \cos \theta e^{jk_0 z_0} \cos \theta \left\{ n^2(0) \begin{vmatrix} v_1(0) & v_2(0) \\ v_1'(0) & v_2'(0) \end{vmatrix} - n^2(z_0) \begin{vmatrix} v_1(z_0) & v_2(z_0) \\ v_1'(z_0) & v_2'(z_0) \end{vmatrix} \right\} \quad (12)$$

From Abel's formula,² the Wronskians of (1) and (2) are, respectively

$$\begin{vmatrix} u_1(z) & u_2(z) \\ u_1'(z) & u_2'(z) \end{vmatrix} = \text{const.};$$

$$\begin{vmatrix} v_1(z) & v_2(z) \\ v_1'(z) & v_2'(z) \end{vmatrix} = \text{const.}$$

$$\times \exp \left(\int_0^z d[\ln n^2(z)] \right)$$

$$= \text{const.} \times \frac{n^2(z)}{n^2(0)}. \quad (13)$$

Therefore,

$$T_{\perp} = T_{\perp}^* \quad T_{\parallel} = T_{\parallel}^* \quad (14)$$

$$R_{\perp} = R_{\perp}^* \quad \text{if} \quad \begin{vmatrix} u_1(0) & u_2(0) \\ u_1'(z_0) & u_2'(z_0) \end{vmatrix}$$

$$= \begin{vmatrix} u_1(z_0) & u_2(z_0) \\ u_1'(0) & u_2'(0) \end{vmatrix}$$

$$R_{\parallel} = R_{\parallel}^* \quad \text{if} \quad n^2(0) \begin{vmatrix} v_1(0) & v_2(0) \\ v_1'(z_0) & v_2'(z_0) \end{vmatrix}$$

$$= n^2(z_0) \begin{vmatrix} v_1(z_0) & v_2(z_0) \\ v_1'(0) & v_2'(0) \end{vmatrix}. \quad (15)$$

Thus, at a given frequency, angle of incidence, and polarization, the transmission of

electromagnetic waves through a one-dimensional inhomogeneous plasma is independent of the direction of transmission. On the other hand, the reflection coefficients, in general, do not necessarily conform to a reciprocity relationship. These results were checked by running a few cases on a computing machine program developed at Langley.

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²F. B. Hildebrand, "Advanced Calculus for Engineers," Prentice-Hall, Inc., Englewood Cliffs, N. J., pp. 31-35; 1957.

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